



**ENGINEERS**  
NEVER STOP LEARNING

# Network Analysis

*是德科技專案經理*

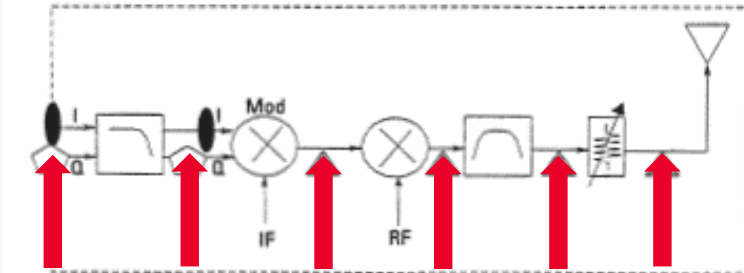
*Keven Chang*

# Agenda

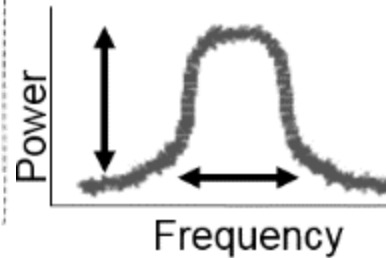
- Transmission Lines and S-Parameters
- Network Analyzer Block Diagram
- Network Analysis Measurements
- Calibration and Error Correction

# Transmit Receive Design Challenges

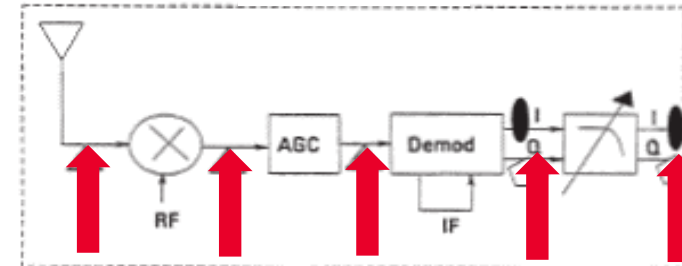
## TRANSMIT



- Output Power
- Operating Frequency
- Environment/Interference
- Noise



## RECEIVE

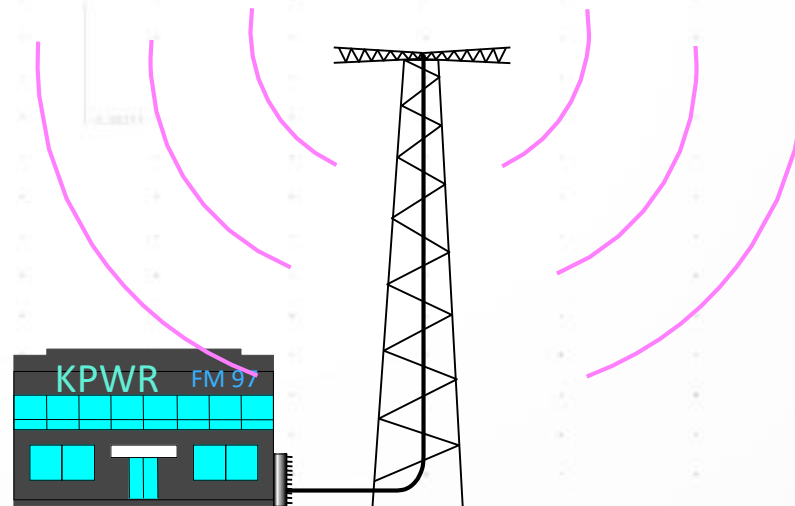


- Sensitivity
- Adjacent Channel Selectivity
- Operating Frequency
- Environment/Interference
- Noise
- Dynamic Range

End goal: maximize link budget, fidelity & efficiency

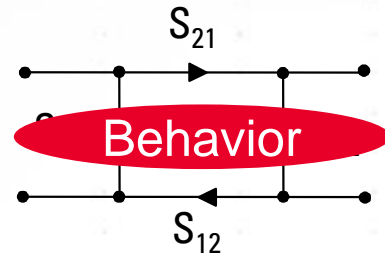
# Why Do We Need to Test Components?

- Verify specifications of “**building blocks**” for more **complex RF systems**
- Ensure **distortion less** transmission of **communications signals**
  - **Linear**: constant amplitude, linear phase / constant group delay
  - **Nonlinear**: harmonics, intermodulation, compression, X-parameters
- Ensure **good match** when absorbing power (e.g., an antenna)

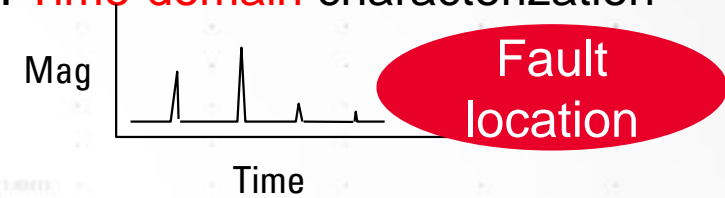


# The Need for Both Magnitude and Phase

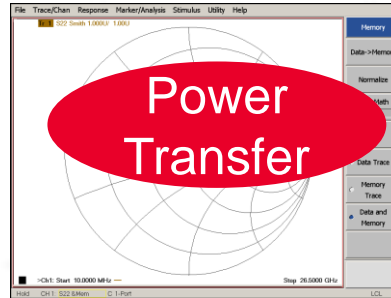
1. Complete characterization of **linear networks**



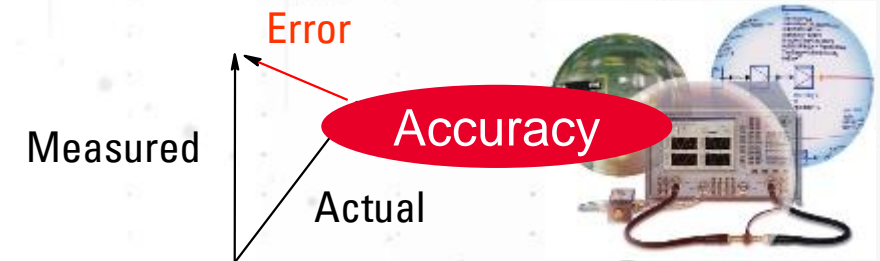
4. **Time-domain** characterization



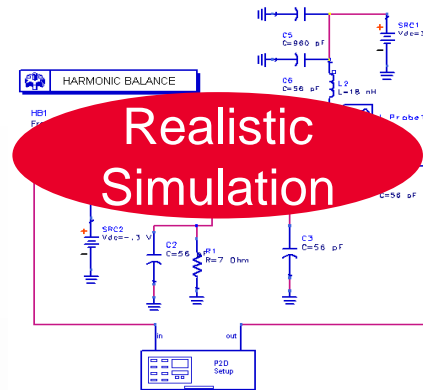
2. Complex impedance needed to design **matching circuits**



5. **Vector-error** correction



3. Complex values needed for **device modeling**

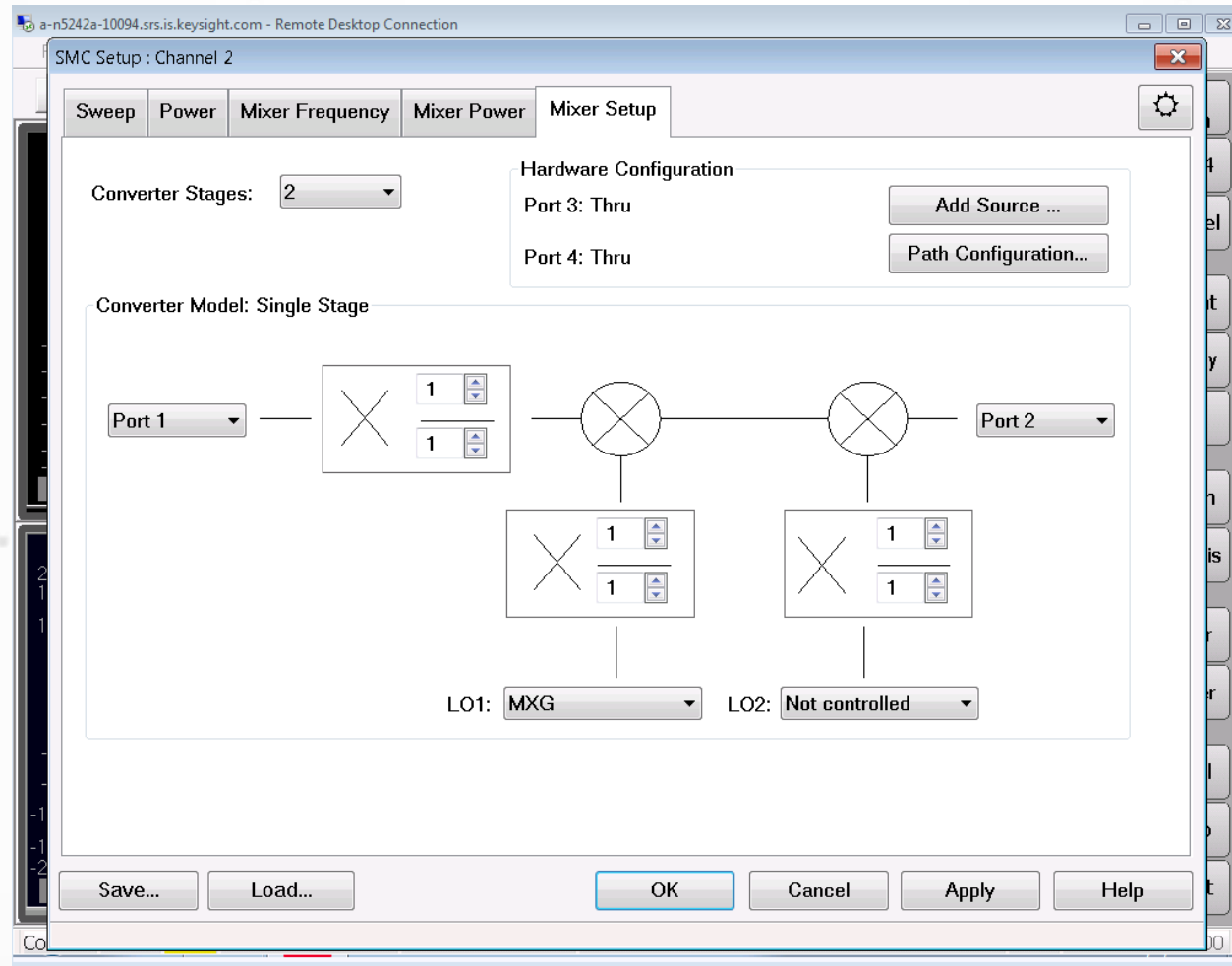


6. **X-parameter (nonlinear)** characterization

**Pre-distortion**

# Mixer Measurement is simplified with UI

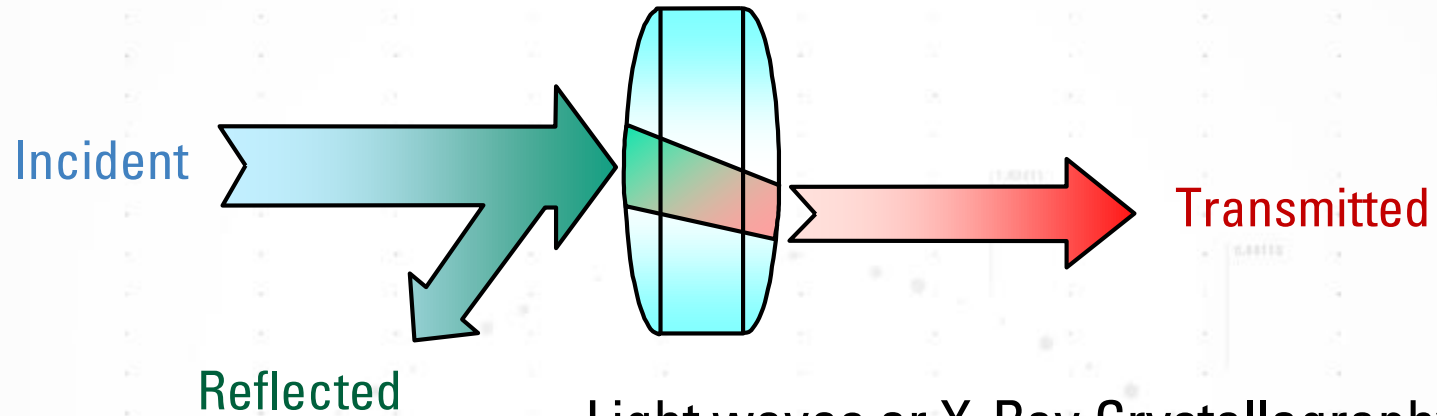
SUPPORTS SINGLE AND DUAL STAGE CONVERTERS.



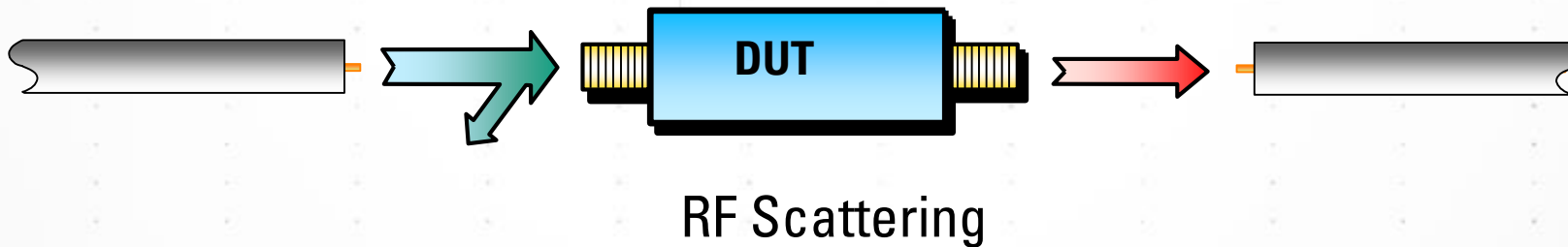
# Agenda

- RF/Microwave Design Challenges
- **Transmission Lines and S-Parameters**
- Network Analyzer Block Diagram
- Network Analysis Measurements
- Calibration and Error Correction

# RF Energy Transmission



Light waves or X-Ray Crystallography  
and X-Ray Scattering

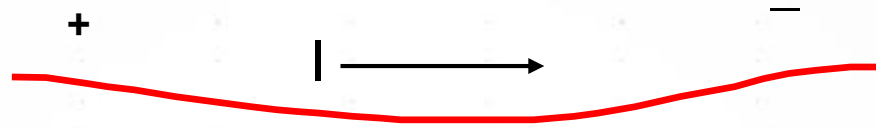




# Transmission Line Basics

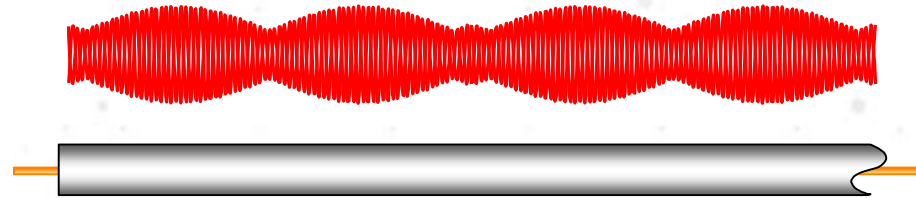
- Low Frequencies

- Wavelengths  $\gg$  wire length
- Current (I) travels down wires easily for efficient power transmission
- Measured voltage and current not dependent on position along wire



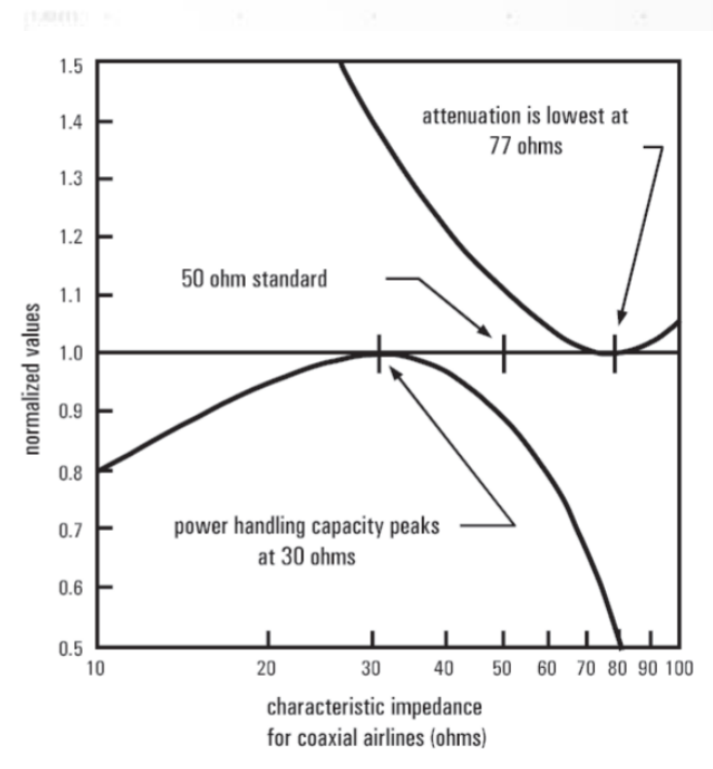
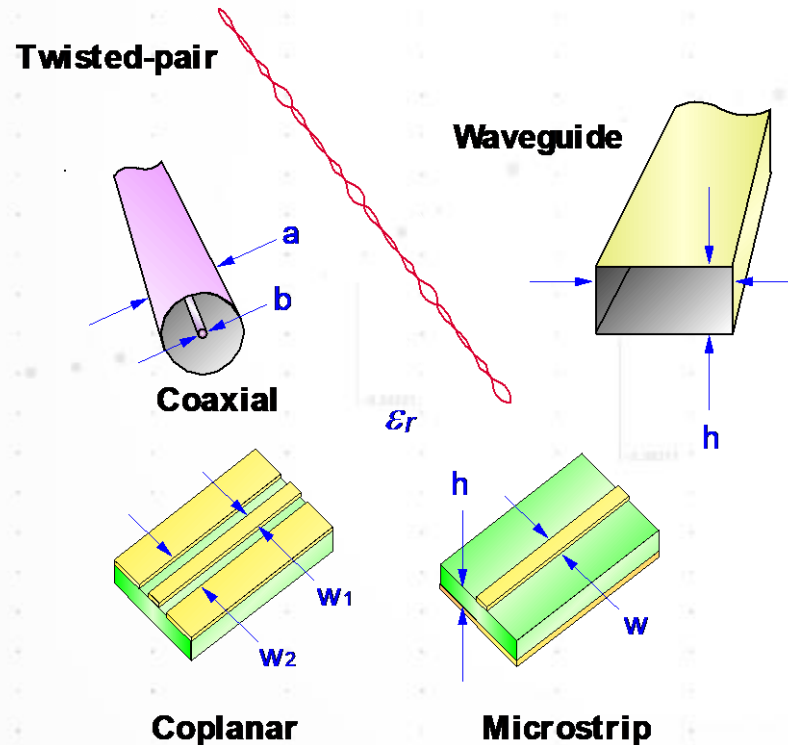
- High Frequencies

- Wavelength  $\sim$  or  $\ll$  length of transmission medium
- Need transmission lines for efficient power transmission
- Matching to characteristic impedance ( $Z_0$ ) is very important for low reflection and maximum power transfer
- Measured envelope voltage dependent on position along line



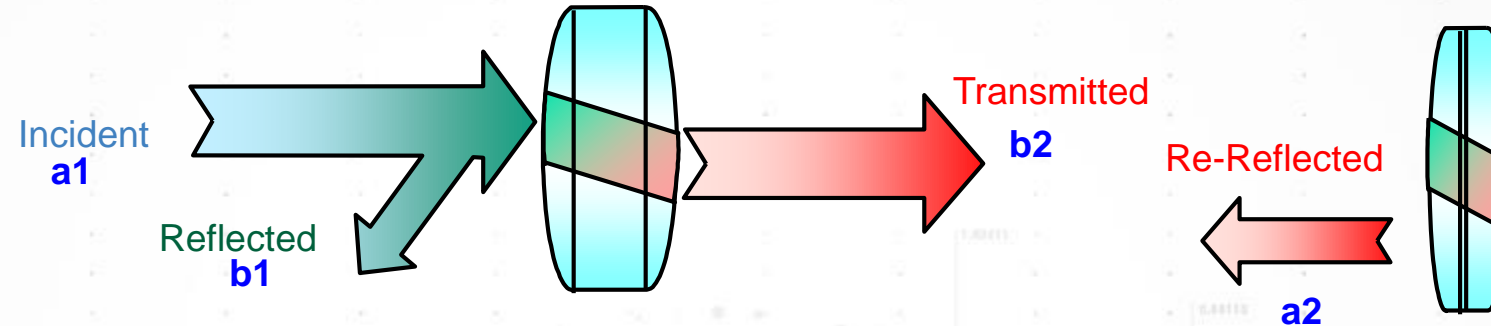
# Transmission line $Z_0$

- $Z_0$  determines relationship between **voltage and current waves**
- $Z_0$  is a function of physical **dimensions and  $\epsilon_r$**
- $Z_0$  is usually a **real impedance (e.g. 50 or 75 ohms)**



For more information on transmission line basics:  
<http://literature.cdn.keysight.com/litweb/pdf/5965-7917E.pdf>

# High-frequency Device Characterization



## REFLECTION

$$\frac{\text{Reflected}}{\text{Incident}} = \frac{b1}{a1}$$

- VSWR
- S-Parameters  $S_{11}, S_{22}$
- Reflection Coefficient  $\Gamma, \rho$
- Impedance, Admittance  $R+jX, G+jB$
- Return Loss

## TRANSMISSION

$$\frac{\text{Transmitted}}{\text{Incident}} = \frac{b2}{a1}$$

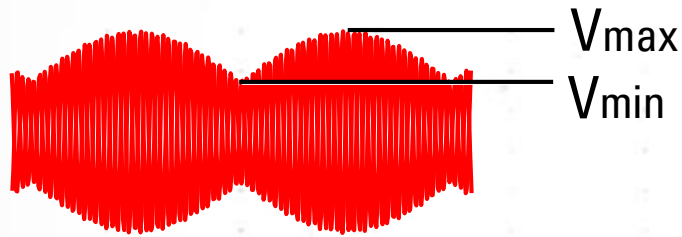
- Gain / Loss
- S-Parameters  $S_{21}, S_{12}$
- Transmission Coefficient  $T, \tau$
- Insertion Phase
- Group Delay

# Reflection Parameters

$$\text{Reflection Coefficient [S11]} = \Gamma = \frac{V_{\text{reflected}}}{V_{\text{incident}}} = \rho \angle \Phi = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$\text{Return loss} = -20 \log(\rho), \quad \rho = |\Gamma|$$

Colloquially: Return loss =  $20 \log(\rho)$ ,

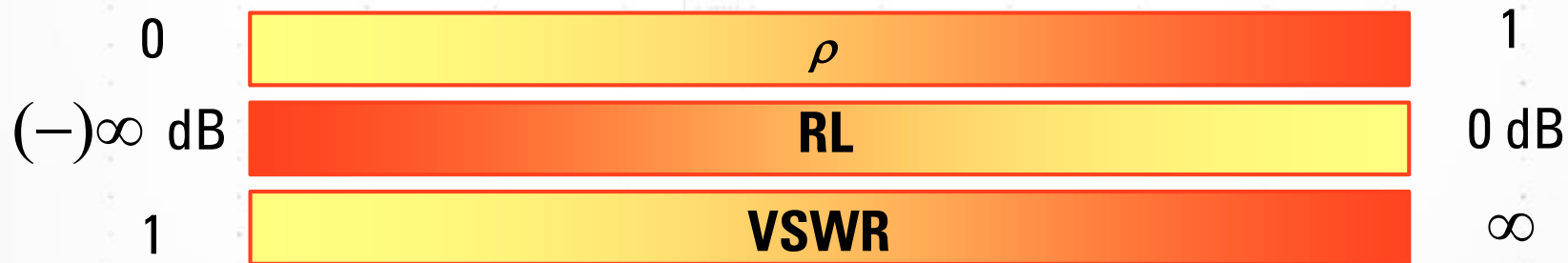


**Voltage Standing Wave Ratio**

$$\text{VSWR} = \frac{V_{\text{max}}}{V_{\text{min}}} = \frac{1 + \rho}{1 - \rho}$$

**No reflection**  
( $Z_L = Z_0$ )

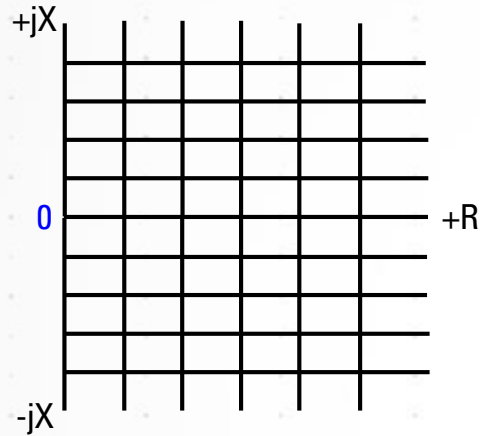
**Full reflection**  
( $Z_L = \text{open, short}$ )



For more information on reflection/transmission parameter basics:  
<http://literature.cdn.keysight.com/litweb/pdf/5965-7917E.pdf>

# Smith Chart Review

QUICKLY AND EASILY GET IMPEDANCE

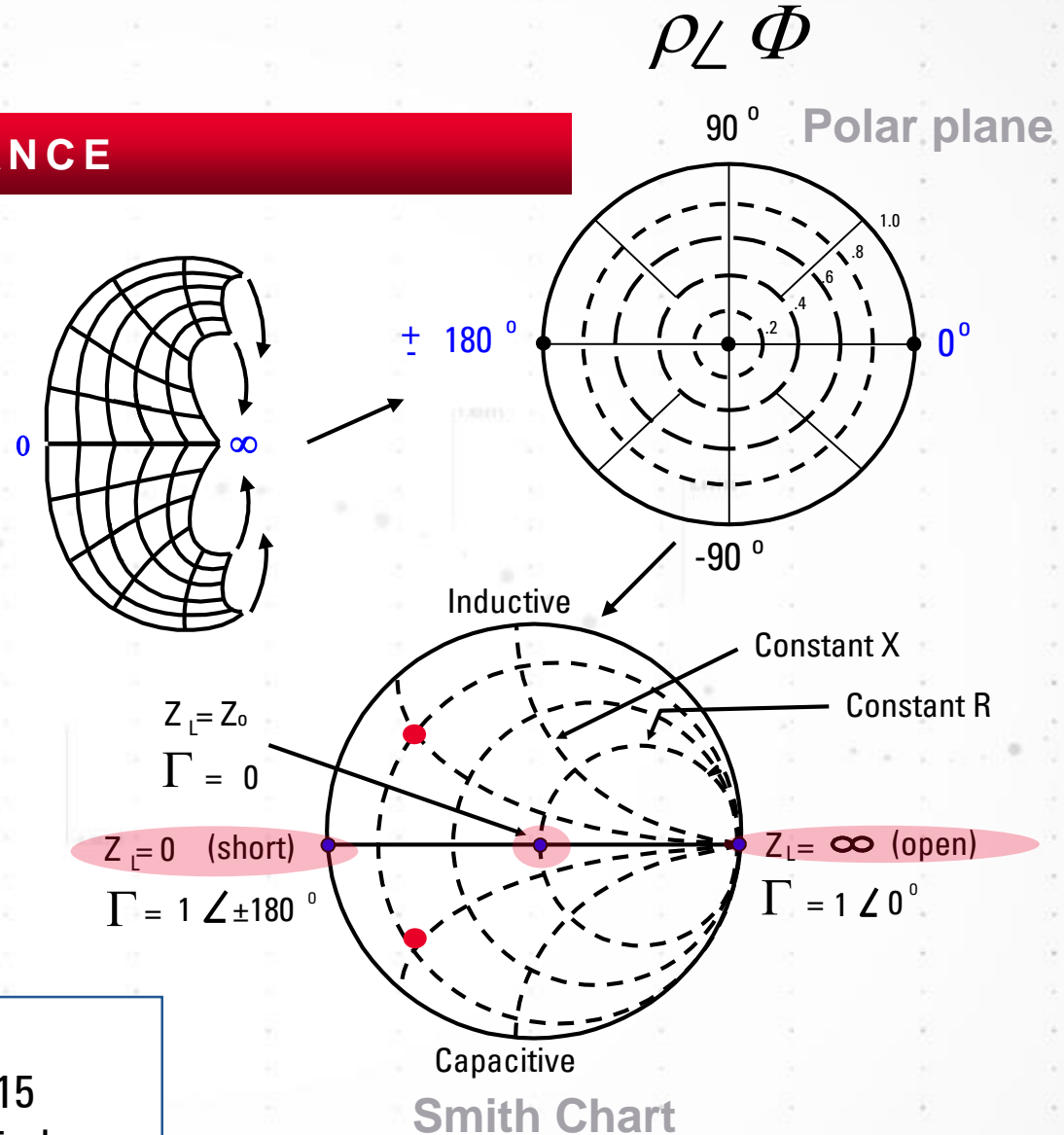


Rectilinear impedance plane

i.e:  $R+jX$ ,

Smith Chart maps  
rectilinear impedance plane  
onto polar plane

Example: in a 50-ohm system,  
a normalized value of  $0.3 - j0.15$   
becomes  $15 - j7.5$  ohms



# Characterizing Unknown Devices

## USING PARAMETERS (H, Y, Z, S) TO CHARACTERIZE DEVICES

- Gives **linear behavioral model** of our device
- Measure parameters (e.g. **voltage and current**) **versus frequency** under various source and **load conditions** (e.g. **short and open circuits**)
- Compute device parameters from measured data
- **Predict circuit performance under any source and load conditions**

### **H-parameters**

$$V_1 = h_{11}I_1 + h_{12}V_2$$

$$I_2 = h_{21}I_1 + h_{22}V_2$$

(Hybrid)

### **Y-parameters**

$$I_1 = y_{11}V_1 + y_{12}V_2$$

$$I_2 = y_{21}V_1 + y_{22}V_2$$

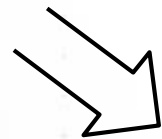
(Admittance)

### **Z-parameters**

$$V_1 = z_{11}I_1 + z_{12}I_2$$

$$V_2 = z_{21}I_1 + z_{22}I_2$$

(Impedance)

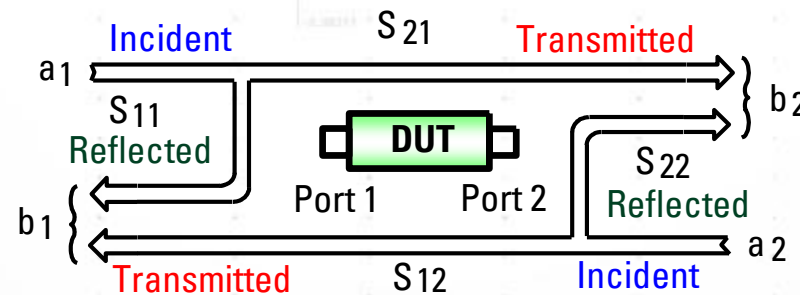


$$h_{11} = \left. \frac{V_1}{I_1} \right|_{V_2=0} \quad (\text{requires } \textit{short circuit})$$

$$h_{12} = \left. \frac{V_1}{V_2} \right|_{I_1=0} \quad (\text{requires } \textit{open circuit})$$

# Why Use Scattering, S-Parameters?

- Relatively easy to **obtain** at **high frequencies**
  - Measure voltage traveling waves with a **vector network analyzer**
  - Don't need **shorts/opens** (can cause active devices to oscillate or self-destruct)
- Relate to **familiar** measurements (gain, loss, reflection coefficient ...)
- Can **cascade S-parameters** of multiple devices to predict system performance
- Can **compute H-, Y-, or Z-parameters** from S-parameters if desired
- Can easily import and use S-parameter files in **electronic-simulation tools**

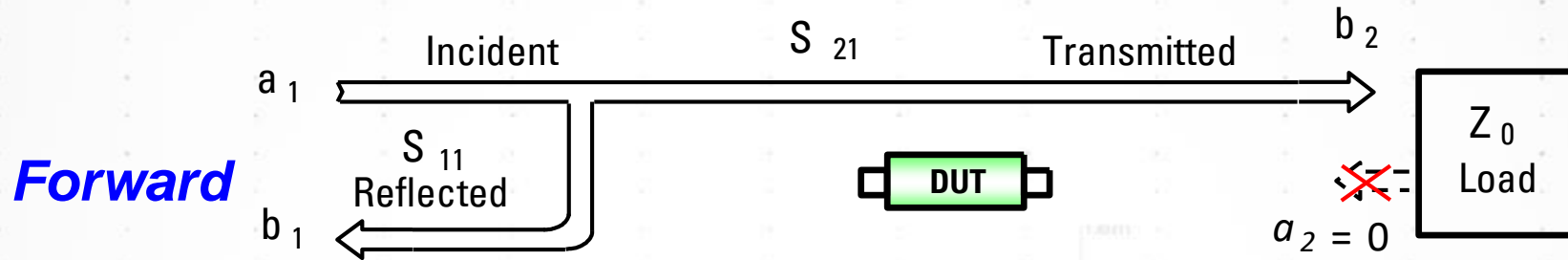


$$b_1 = S_{11} a_1 + S_{12} a_2$$

$$b_2 = S_{21} a_1 + S_{22} a_2$$

Component Test Fundamentals

# Measuring S-Parameters

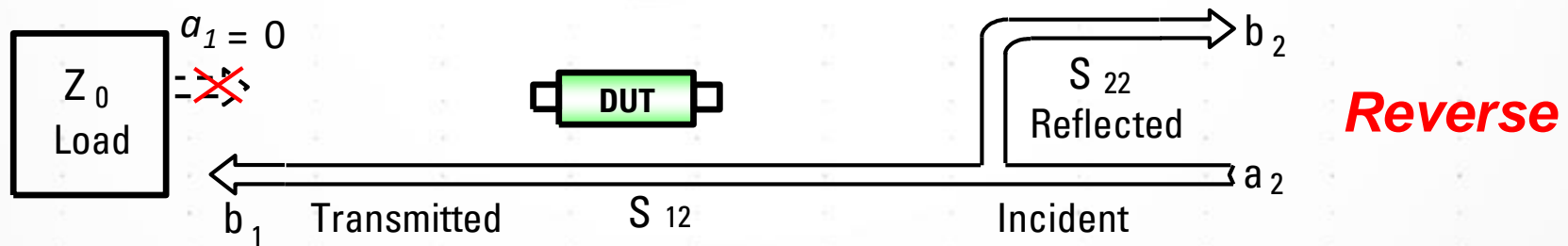


$$S_{11} = \frac{\text{Reflected}}{\text{Incident}} = \frac{b_1}{a_1} \Big|_{a_2 = 0}$$

$$S_{21} = \frac{\text{Transmitted}}{\text{Incident}} = \frac{b_2}{a_1} \Big|_{a_2 = 0}$$

$$S_{22} = \frac{\text{Reflected}}{\text{Incident}} = \frac{b_2}{a_2} \Big|_{a_1 = 0}$$

$$S_{12} = \frac{\text{Transmitted}}{\text{Incident}} = \frac{b_1}{a_2} \Big|_{a_1 = 0}$$





# Equating S-Parameters With Common Measurement Terms



$S_{11}$  = forward reflection coefficient (*input match*)

$S_{22}$  = reverse reflection coefficient (*output match*)

$S_{21}$  = forward transmission coefficient (*gain or loss*)

$S_{12}$  = reverse transmission coefficient (*isolation*)

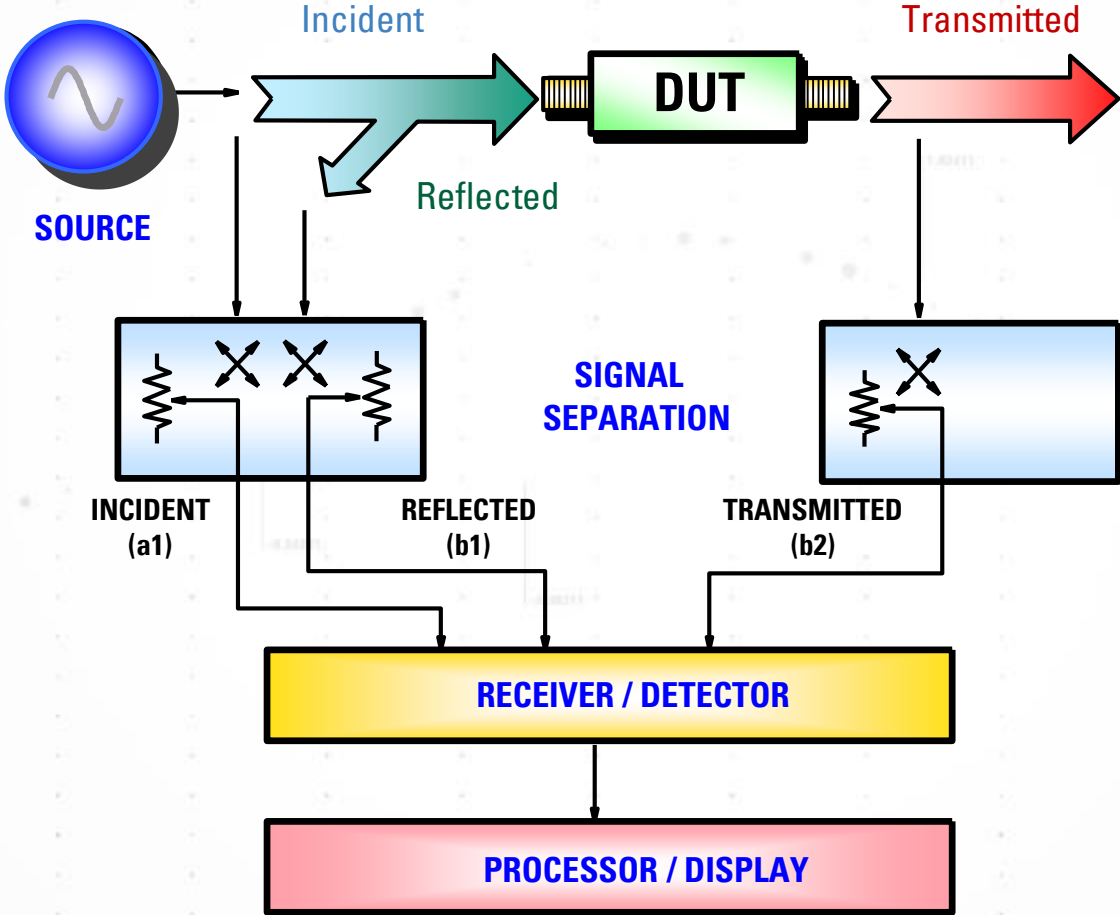
**Remember S-parameters are inherently complex, linear quantities – however, we often express them in a log-magnitude format**

# Agenda

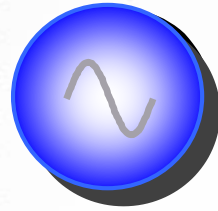
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- **Network Analyzer Block Diagram**
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# Generalized Network Analyzer Block Diagram

FORWARD MEASUREMENTS SHOWN



# Source



- **Source stimulus** can **sweep frequency or power or phase**
- Modern NAs may have the option for **a second internal source** and/or the ability to control external source

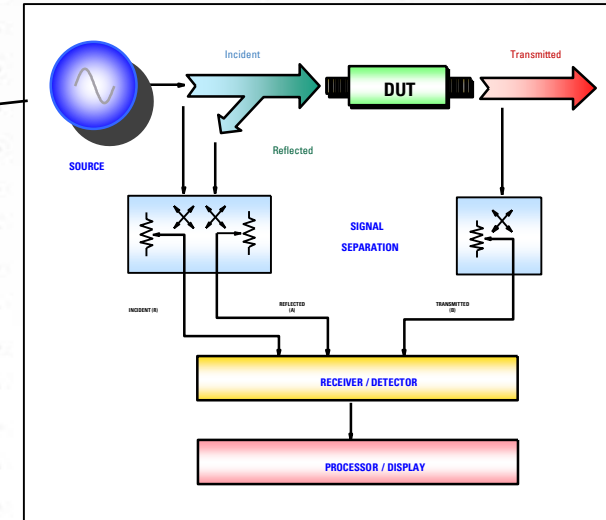
Used for driving differential devices

Can control an internal or external source

as a local oscillator (LO) signal for **mixers and converters**

Useful for mixer measurements

like **conversion loss, group delay**

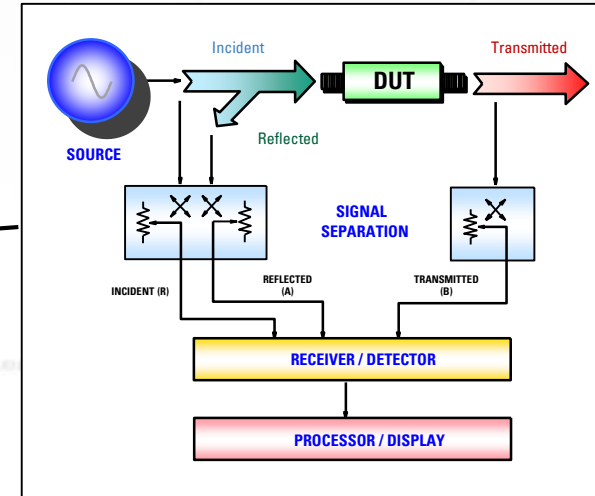


For more information on converter testing:

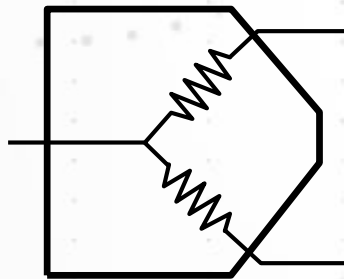
[http://www.keysight.com/upload/cmc\\_upload/All/PNA\\_Advances\\_Converter\\_Testing.pdf](http://www.keysight.com/upload/cmc_upload/All/PNA_Advances_Converter_Testing.pdf)

# Signal Separation

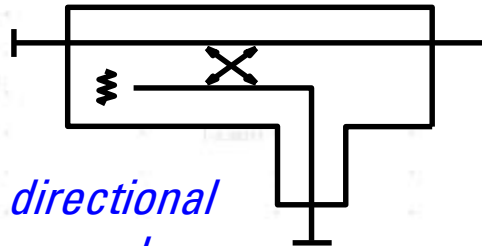
- Measure incident signal for reference
- Separate incident and reflected signal



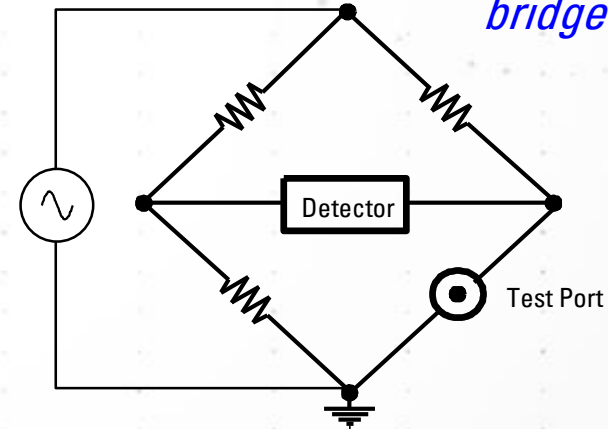
*splitter*



*directional coupler*



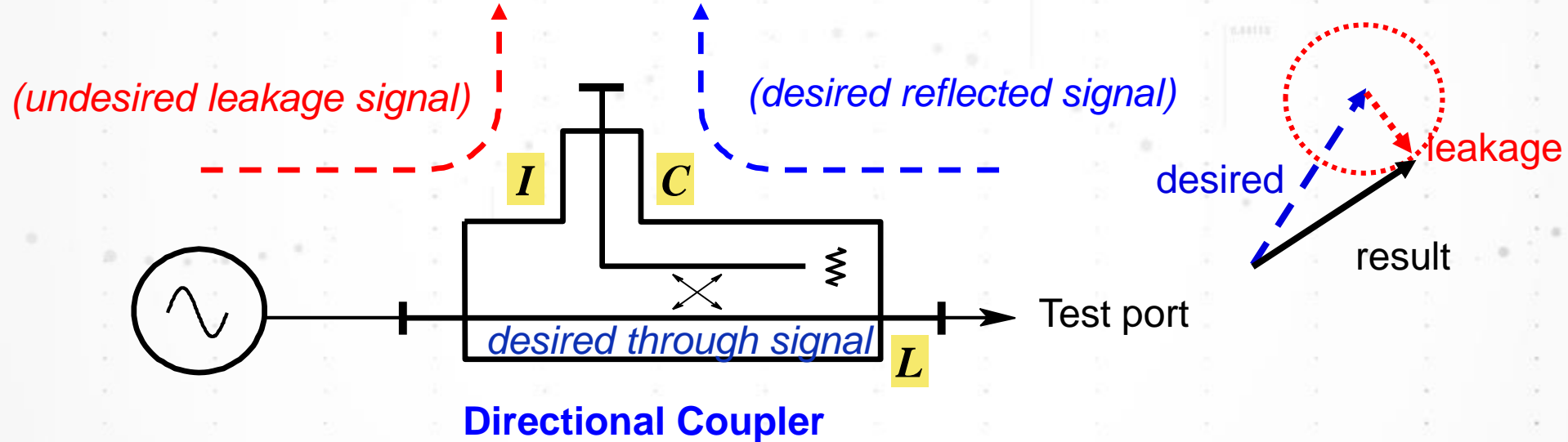
*bridge*



# Directional Coupler & Directivity



- **Directivity** is a measure of how well a directional coupler or bridge can separate signals moving in opposite directions

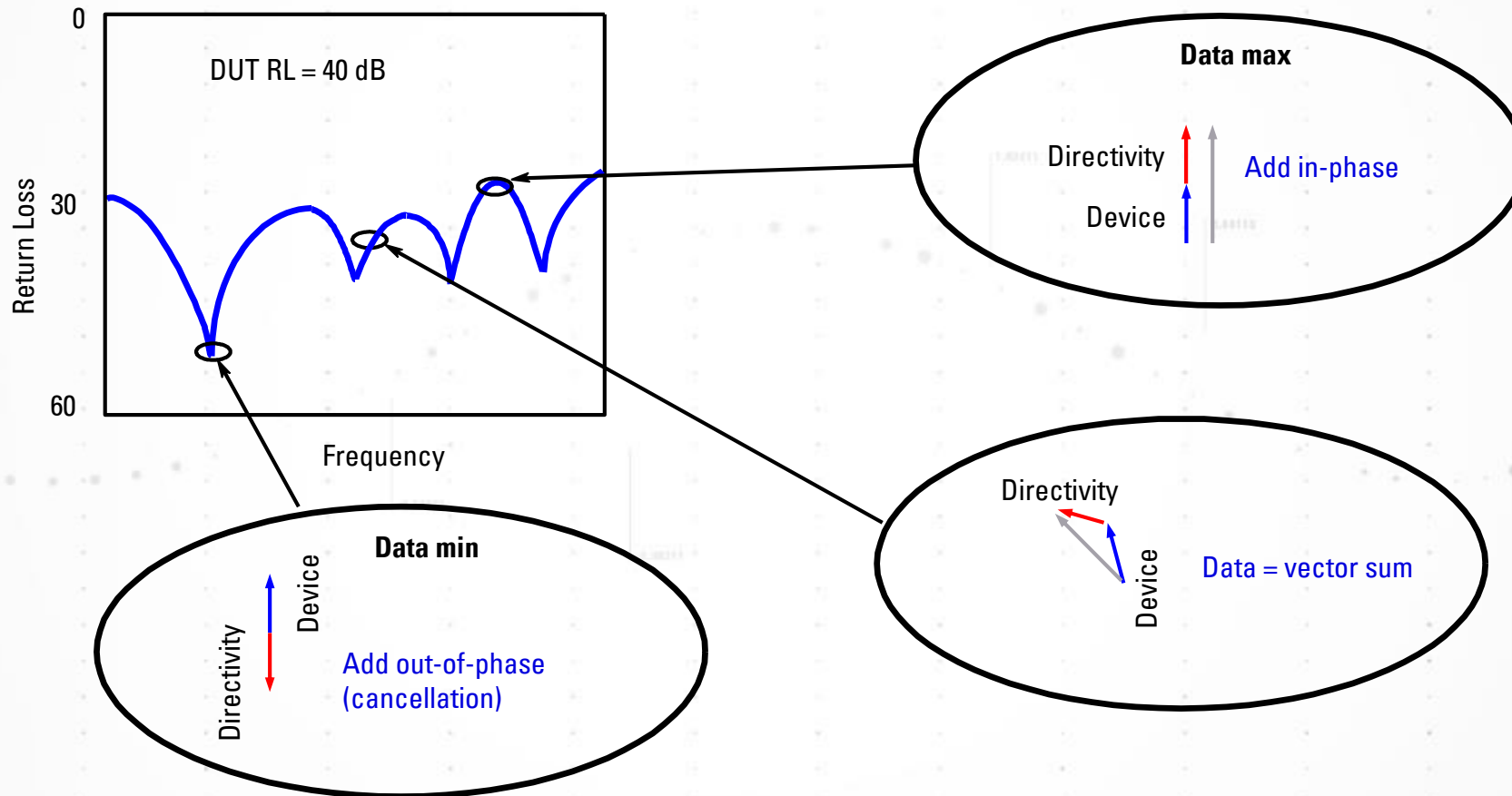


$$\text{Directivity} = \text{Isolation (I)} - \text{Fwd Coupling (C)} - \text{Main Arm Loss (L)}$$

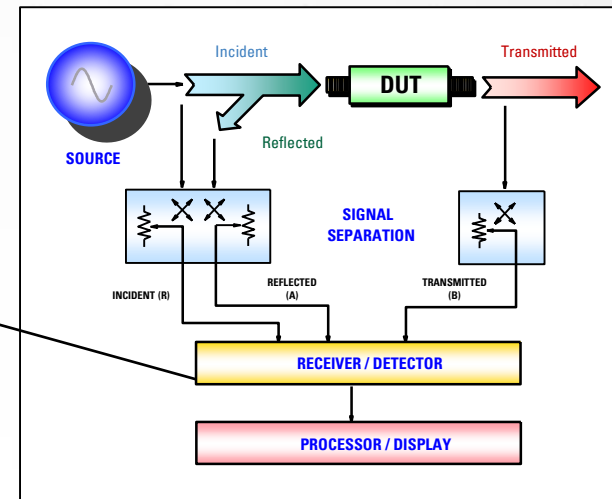
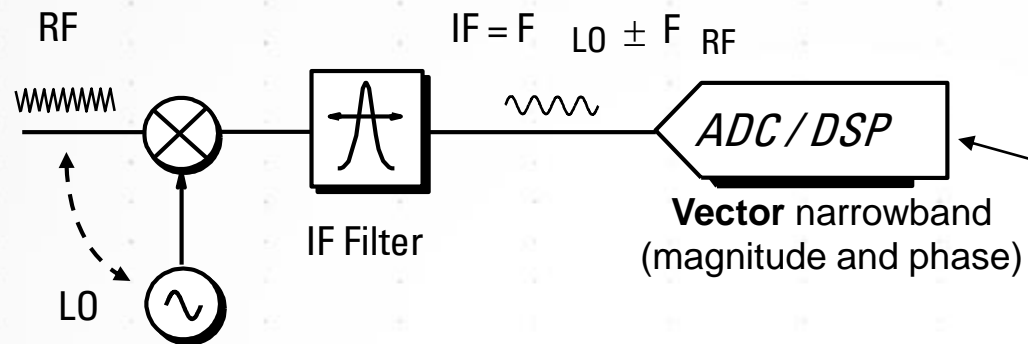
$$\text{Directivity} = 50 \text{ dB (I)} - 20\text{dB(C)} - 1 \text{ dB(L)} = 29 \text{ dB}$$

# Interaction of Directivity with the DUT

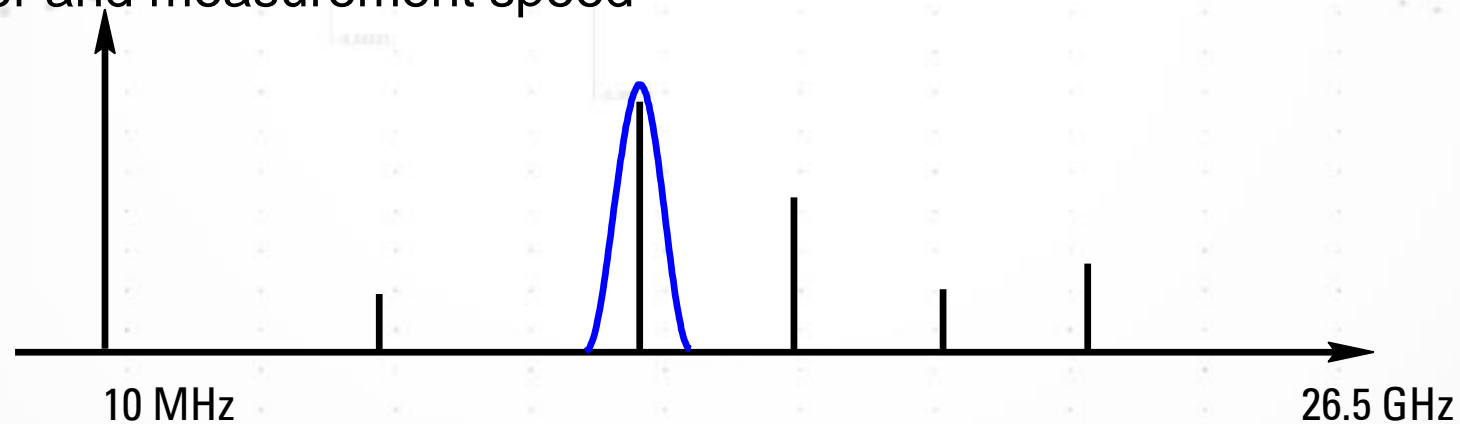
(WITHOUT ERROR CORRECTION)



# Narrowband Detection - Tuned Receiver



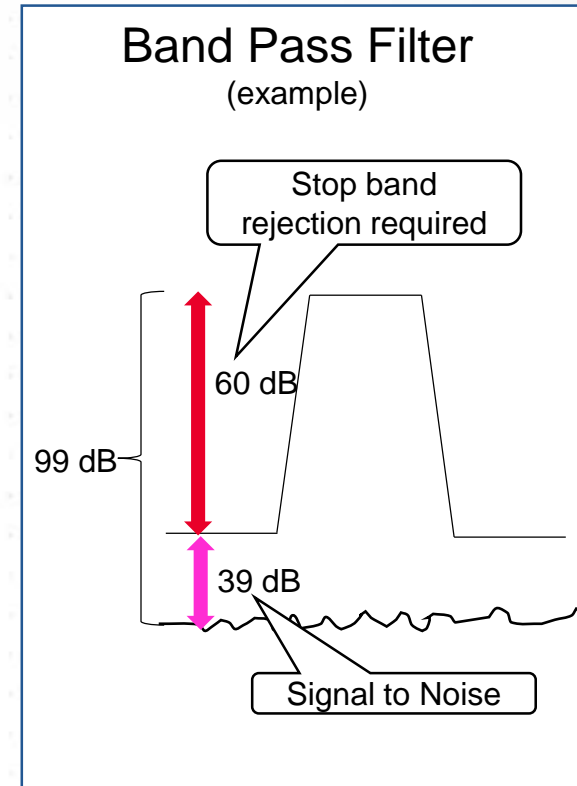
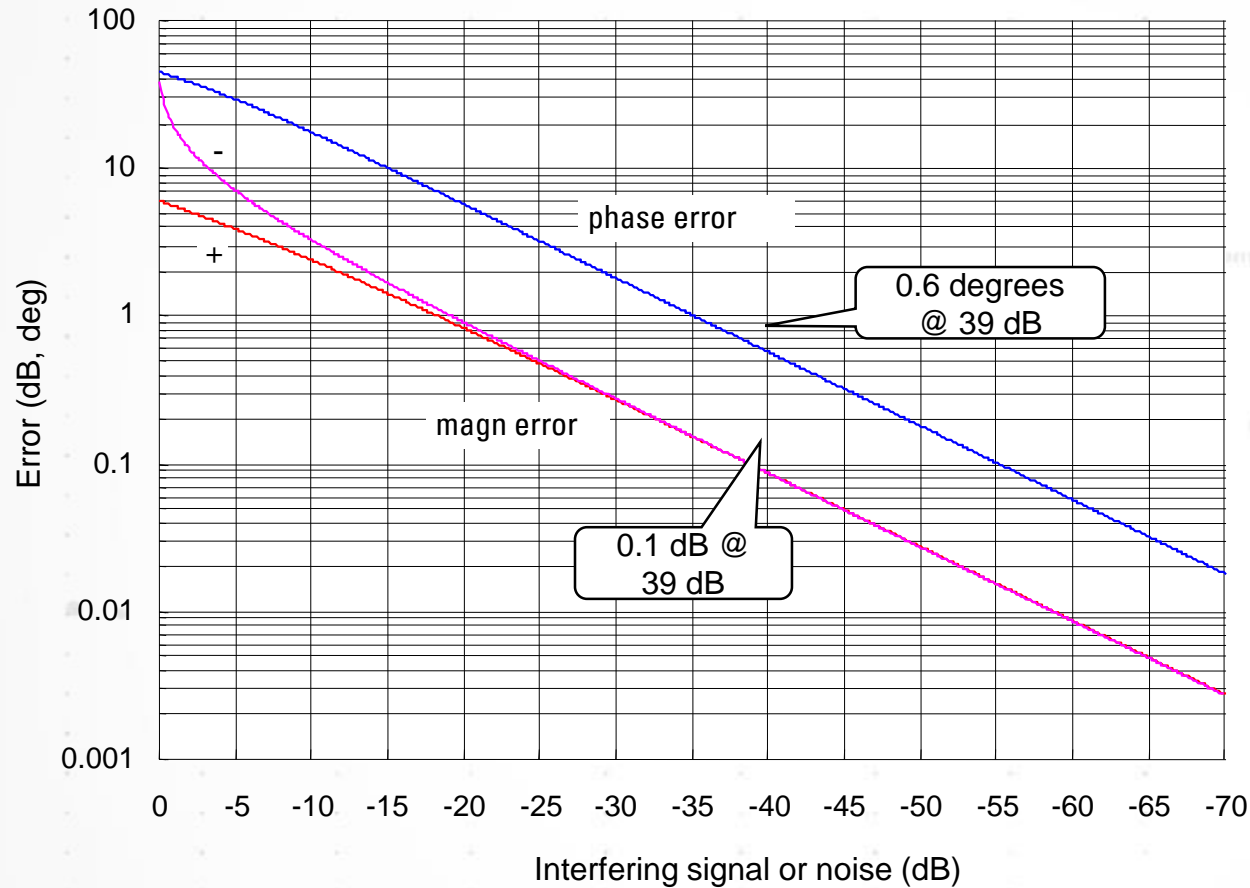
- Best sensitivity / dynamic range
- Provides harmonic / spurious signal rejection
- Improve dynamic range by increasing power, decreasing IF bandwidth, or averaging
- Trade off noise floor and measurement speed





# Dynamic Range and Accuracy

## ERROR DUE TO INTERFERING SIGNAL

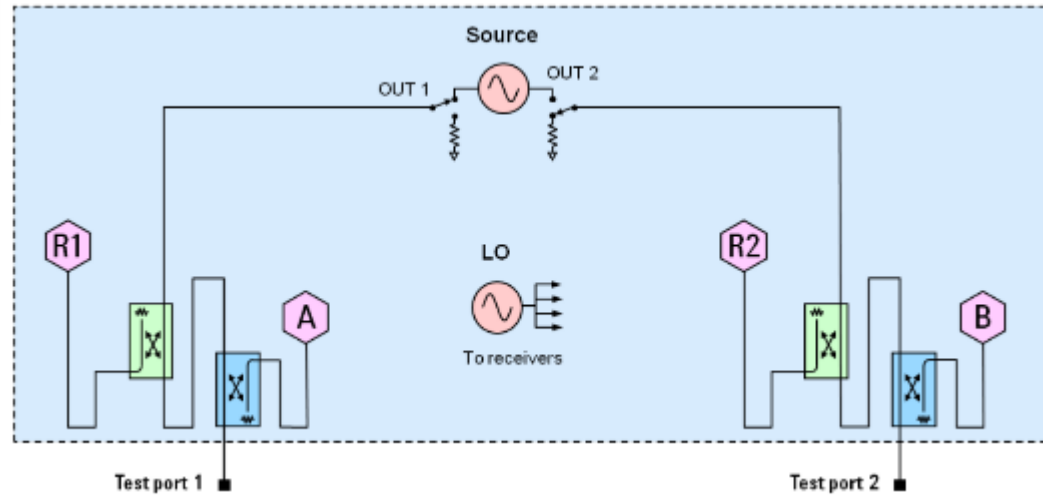


Dynamic range for 0.1 dB accuracy = 60 dB (rejection) + 39 dB (SNR) = 99 dB

*Dynamic range is very important for measurement accuracy!*

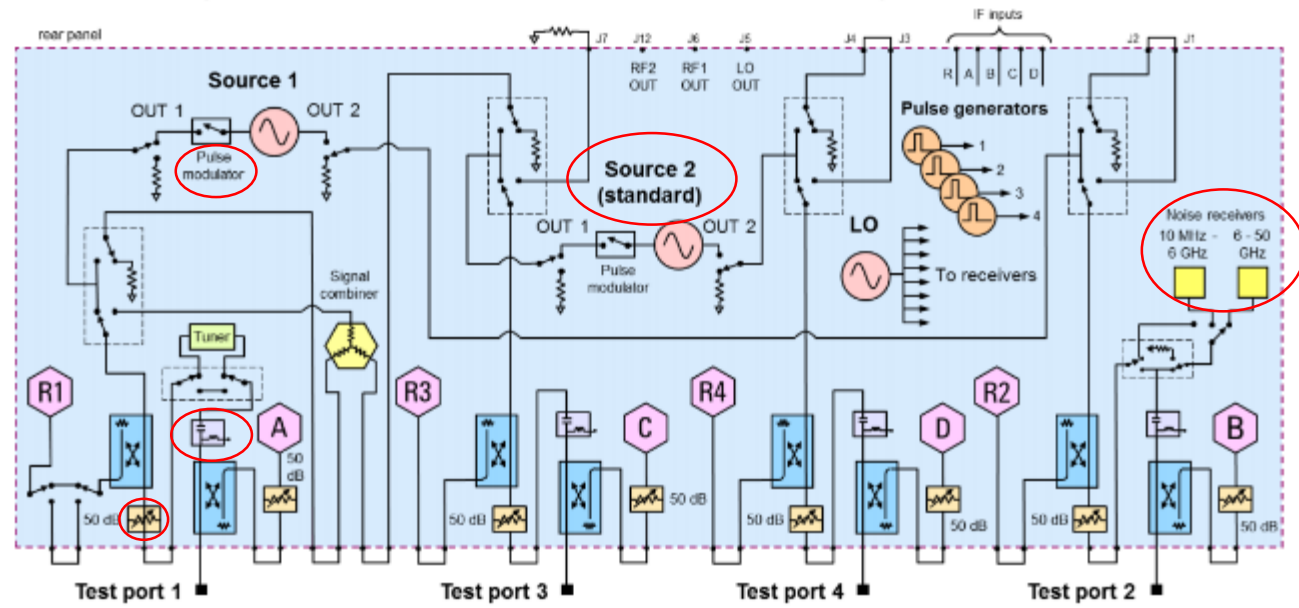
# VNA Block Diagram Examples

- Basic 2 Port

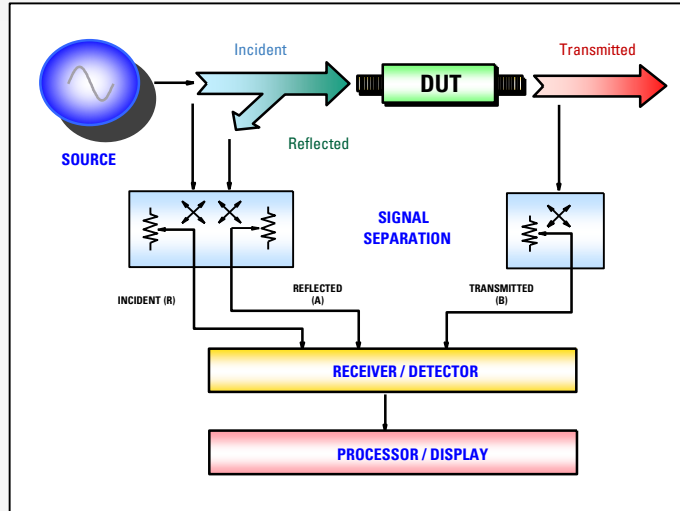


- Performance 4 Port

- Access loops & switches
- 2 sources & combiner
- Pulse modulation
- Noise tuner & LNA receiver
- Attenuators
- Bias-T's



# Processor / Display



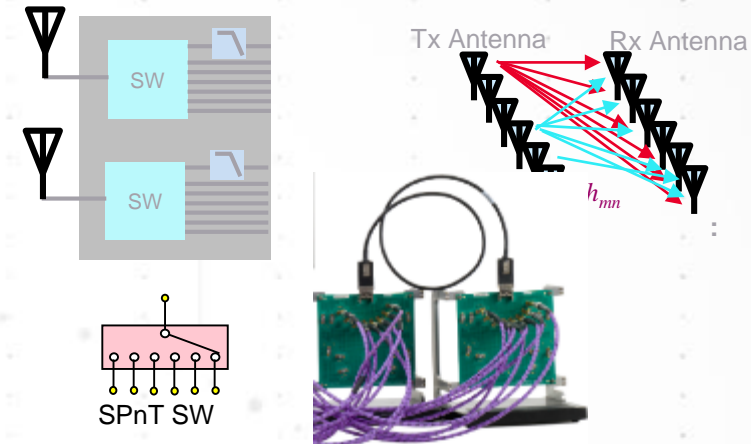
- Markers
- Limit lines
- Pass/fail indicators
- Linear/log formats
- Grid/polar/Smith charts
- Time-domain transform
- Trace math



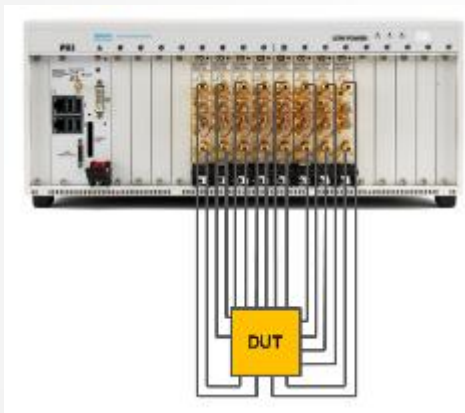
# Multiport Measurement Architectures

## Application Examples

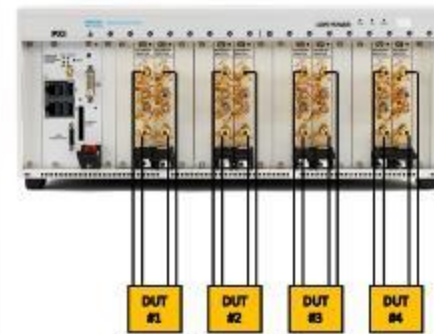
- RF front end modules / antenna switch modules
- Channel measurements of MIMO antennas
- Interconnects (ex. cables, connectors)
- General-purpose multiport devices



## PXI Multiport VNA



## PXI Multi-site VNA



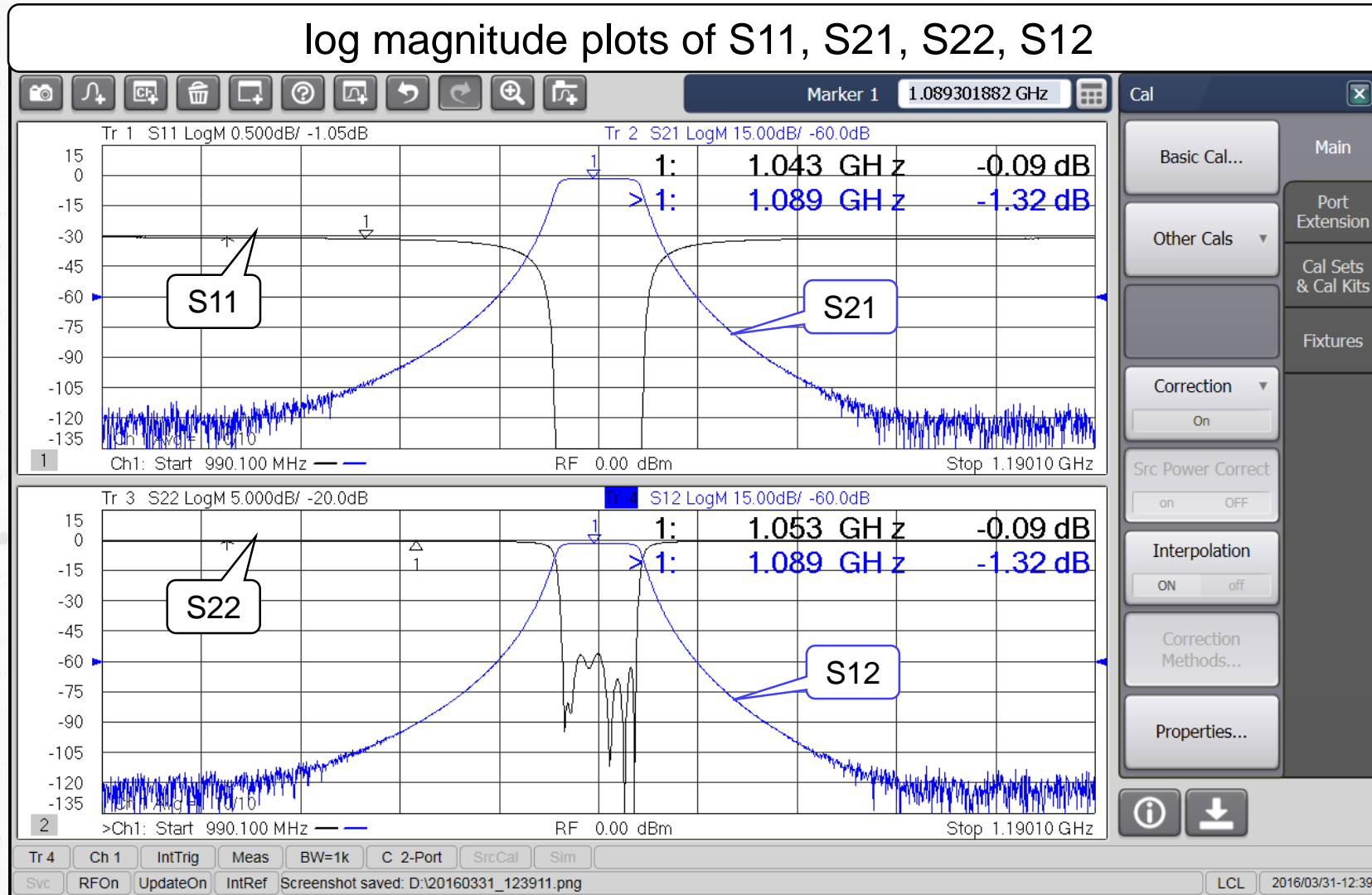
## Key Features

- True multiport VNA with independent modules
- Improved throughput
- High performance without external switches
- Full N-port correction
- Reconfigurable to multiport or multisite

# Agenda

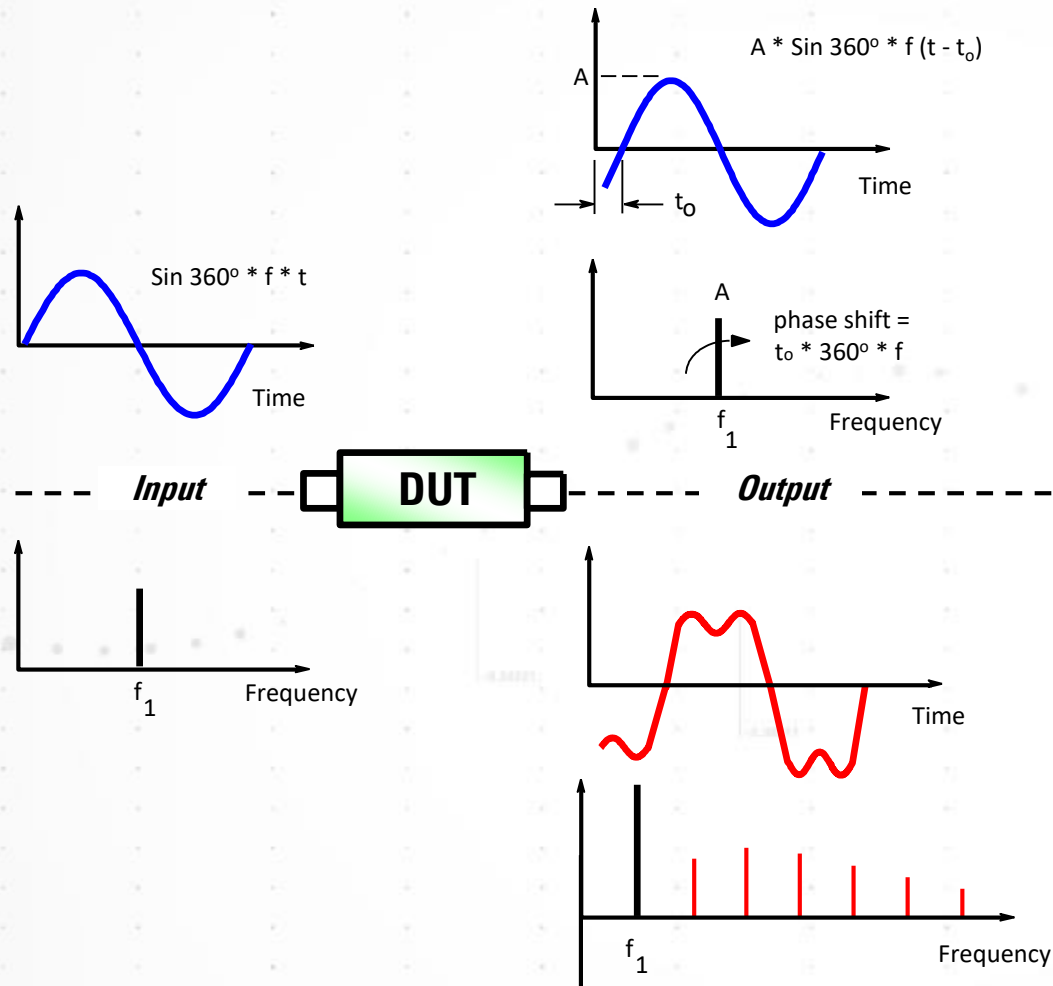
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# Bandpass Filter four S-Parameters





# Linear Versus Nonlinear Behavior



## Linear behavior:

Input and output frequencies are the same (no additional frequencies created)

Output frequency only undergoes magnitude and phase change

## Nonlinear behavior:

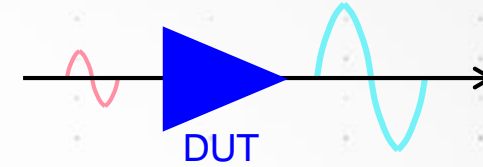
Output frequency may undergo frequency shift (e.g. with mixers)

Additional frequencies created (harmonics, intermodulation)

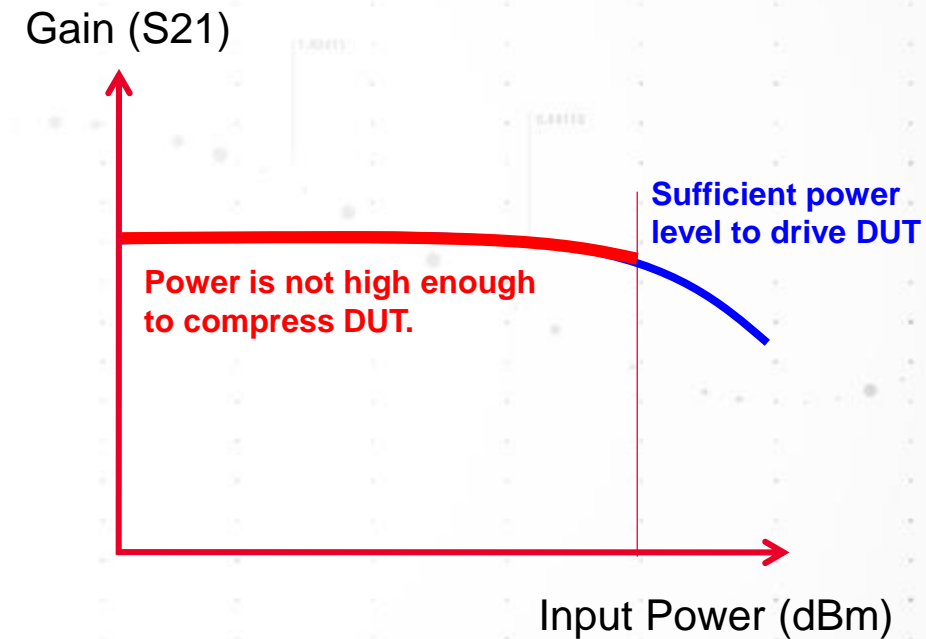
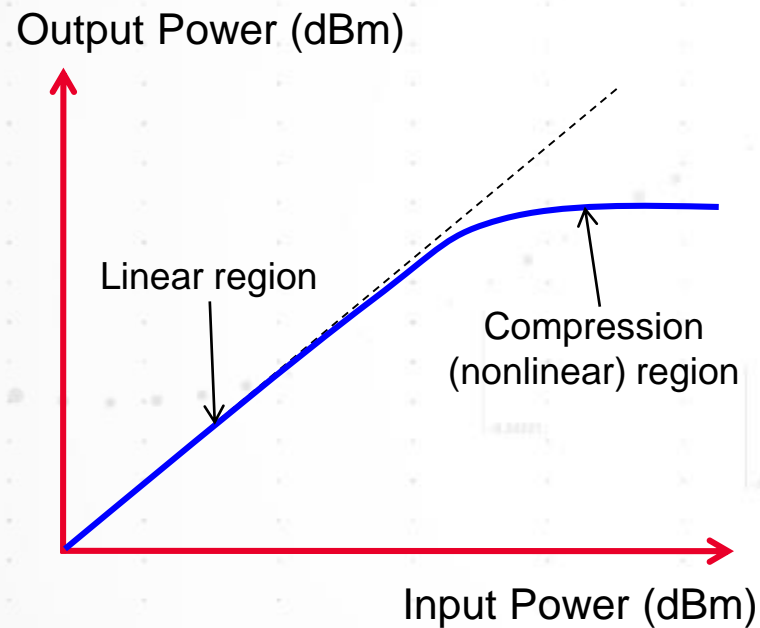
For more information on linear vs. non-linear basics:

<http://literature.cdn.keysight.com/litweb/pdf/5965-7917E.pdf>

# Gain Compression



- Parameter to define the transition between the linear and nonlinear region of an active device.
- The compression point is observed as x dB drop in the gain with VNA's power sweep.

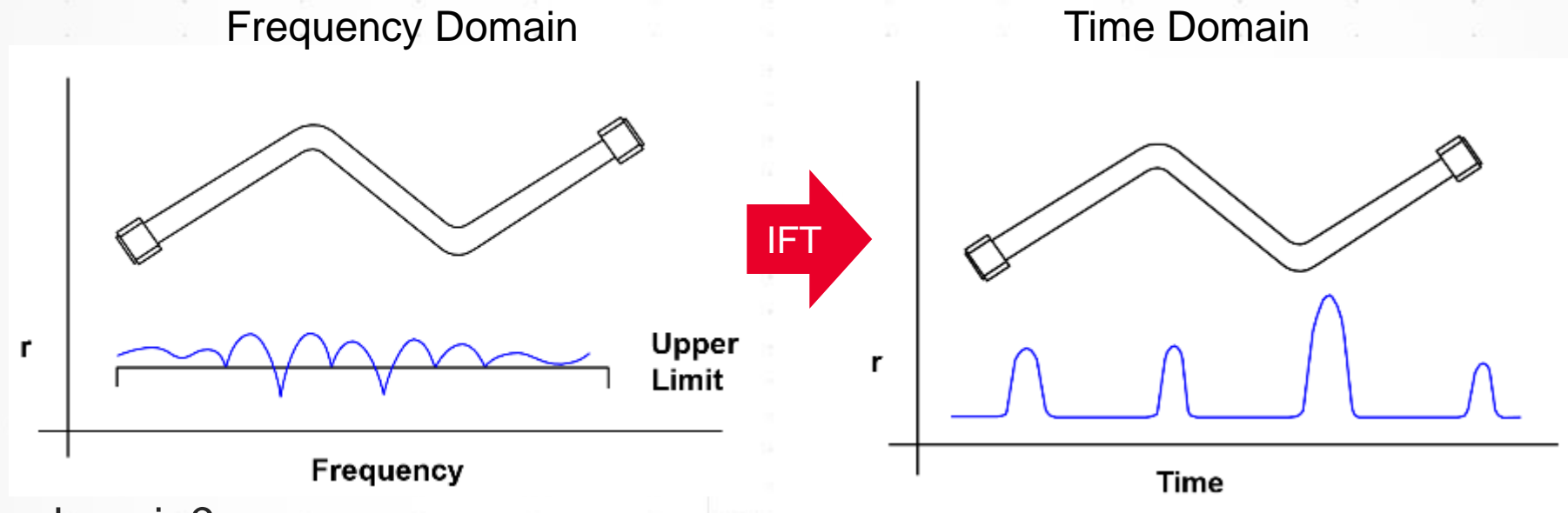


Enough margin of source power capability is needed for analyzers.



# Time vs. Frequency Domain

## S<sub>11</sub> RESPONSE OF SEMIRIGID COAX CABLE



- Why time domain?
  - Locate faults
  - Identify passive or inductive circuit elements
  - Identify and remove unwanted fixture responses
  - And more...

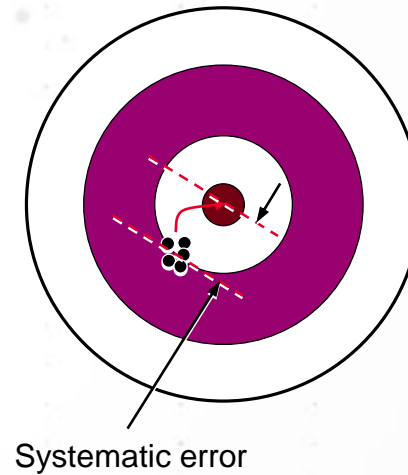
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<http://literature.cdn.keysight.com/litweb/pdf/5989-5723EN.pdf?id=923465>

# Agenda

- RF/Microwave Design Challenges
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# The Need For Calibration

- **Why do we have to calibrate?**
  - It is impossible to make **perfect hardware**
  - It would be extremely difficult and expensive to make **hardware good enough** to entirely eliminate the **need for error correction**
- **How do we get accuracy?**
  - With **vector-error-corrected calibration**
  - **Not** the same as the **yearly instrument calibration**
- **What does calibration do for us?**
  - Removes the largest contributor to **measurement uncertainty: systematic errors**
  - Provides best picture of **true performance of DUT**



# Measurement Error Modeling

- **Systematic Errors**



- Due to imperfections in the analyzer and test setup
- Assumed to be time invariant (predictable)
- Generally, are largest sources of error

- **Random Errors**

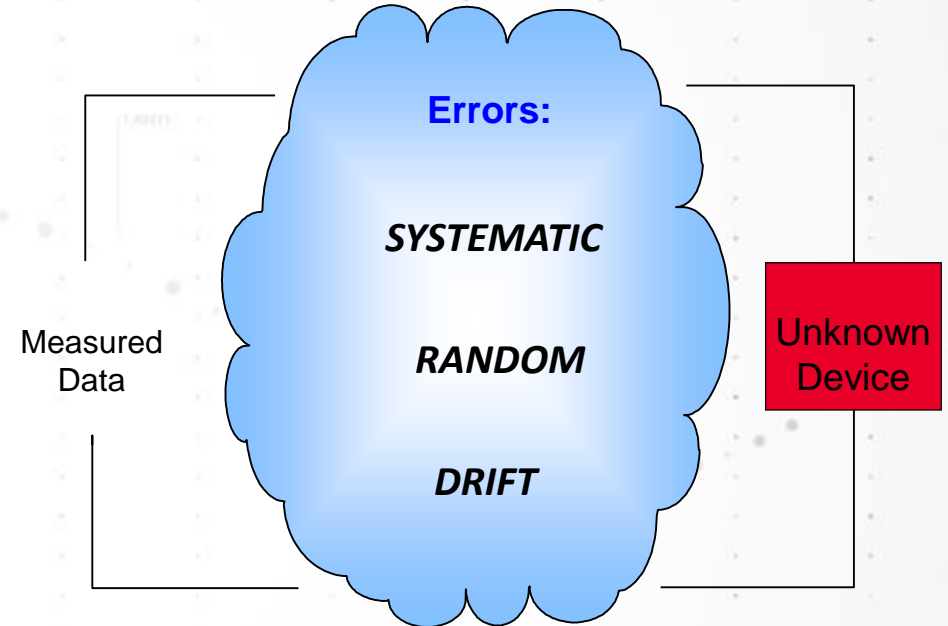


- Vary with time in random fashion (unpredictable)
- Main contributors: instrument noise, switch and connector repeatability

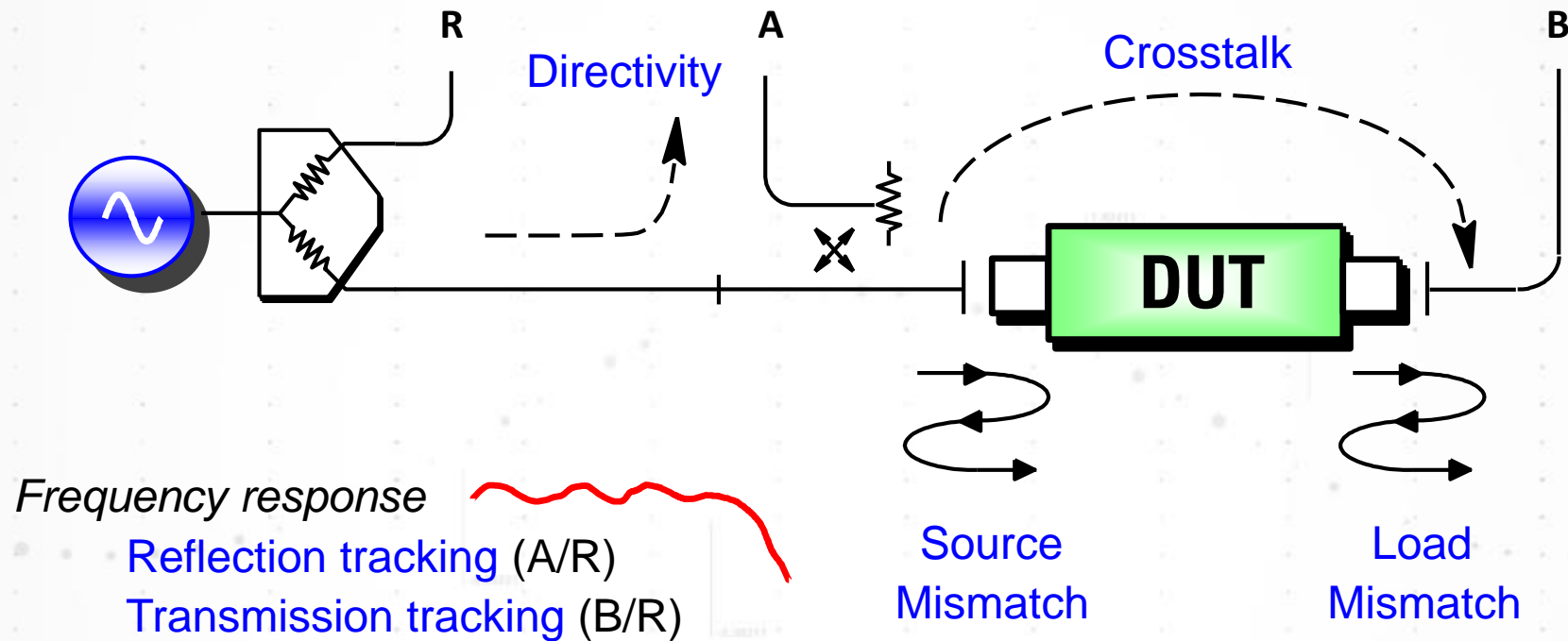
- **Drift Errors**



- Due to system performance changing **after** a calibration has been done
- Primarily caused by **temperature variation**



# Systematic Measurement Errors

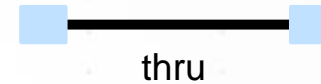


**Six forward and six reverse error terms yields 12 error terms for two-port devices**

# Types of Error Correction

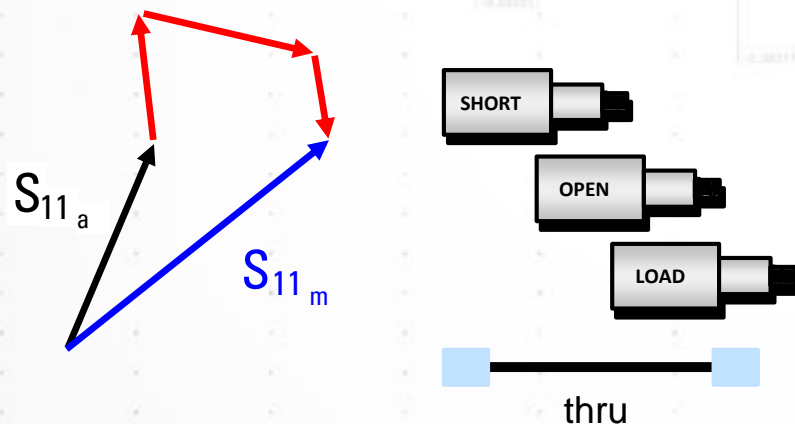
- **Response (normalization)**

- Simple to perform
- Only corrects for tracking (frequency response) errors
- Stores reference trace in memory, then does data divided by memory



- **Vector**

- Requires more calibration standards
- Requires an analyzer that can measure phase
- Accounts for all major sources of systematic error



## Available Standards

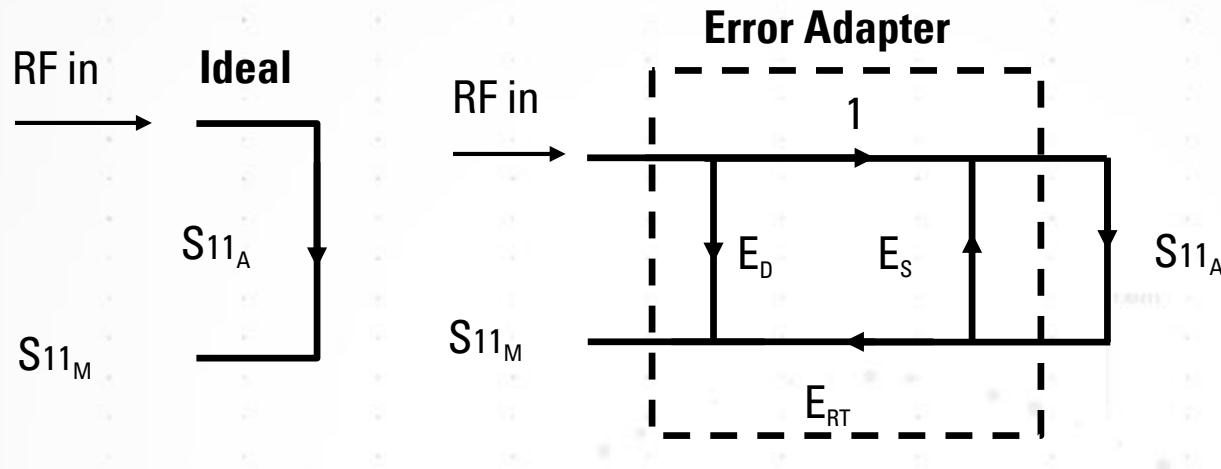


Mechanical short, open, load, thru (SOLT)



Electronically switched arbitrary known impedances

# Reflection: One-Port Vector Error Model



$E_D$  = Directivity

$E_{RT}$  = Reflection tracking

$E_S$  = Source Match

$S_{11M}$  = Measured

$S_{11A}$  = Actual

- To solve for error terms, we measure **3 standards** to generate **3 equations** and **3 unknowns**

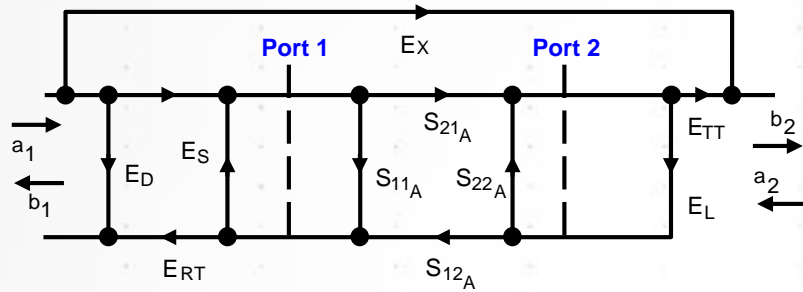
$$S_{11M} = E_D + E_{RT}$$

$$\left[ \frac{S_{11A}}{1 - E_S S_{11A}} \right]$$

- Assumes good termination at port two if testing two-port devices
- If using port two of NA *and* DUT reverse isolation is low (e.g., filter passband):
  - Assumption of good termination is not valid
  - Two-port error correction yields better results

# Two Port 12-term Error Model

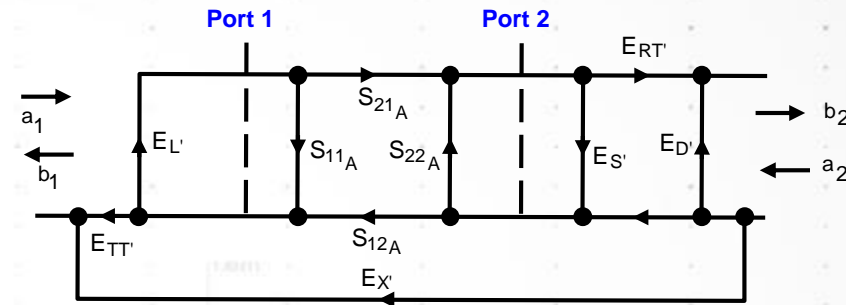
Forward model



|                                     |                                       |
|-------------------------------------|---------------------------------------|
| $E_D$ = fwd directivity             | $E_L$ = fwd load match                |
| $E_S$ = fwd source match            | $E_{TT}$ = fwd transmission tracking  |
| $E_{RT}$ = fwd reflection tracking  | $E_X$ = fwd isolation                 |
| $E_{D'}$ = rev directivity          | $E_{L'}$ = rev load match             |
| $E_{S'}$ = rev source match         | $E_{TT'}$ = rev transmission tracking |
| $E_{RT'}$ = rev reflection tracking | $E_{X'}$ = rev isolation              |

- Each actual S-parameter is a function of all four measured S-parameters
- Analyzer must make forward and reverse sweep to update any one S-parameter
- Luckily, you don't need to know these equations to use a network analyzer
- Crosstalk term, in most cases is not used

Reverse model



$$S_{11A} = \frac{S_{11N} \cdot (1 + S_{22N} \cdot ESR) - ELF \cdot S_{21N} \cdot S_{12N}}{(1 + S_{11N} \cdot ESF)(1 + S_{22N} \cdot ESR) - ELF \cdot ELR \cdot S_{21N} \cdot S_{12N}}$$

$$S_{21A} = \frac{S_{21N} \cdot (1 + S_{22N} \cdot [ESR - ELF])}{(1 + S_{11N} \cdot ESF)(1 + S_{22N} \cdot ESR) - ELF \cdot ELR \cdot S_{21N} \cdot S_{12N}}$$

$$S_{12A} = \frac{S_{12N} \cdot (1 + S_{11N} \cdot [ESF - ELR])}{(1 + S_{11N} \cdot ESF)(1 + S_{22N} \cdot ESR) - ELF \cdot ELR \cdot S_{21N} \cdot S_{12N}}$$

$$S_{22A} = \frac{S_{22N} \cdot (1 + S_{11N} \cdot ESF) - ELR \cdot S_{21N} \cdot S_{12N}}{(1 + S_{11N} \cdot ESF)(1 + S_{22N} \cdot ESR) - ELF \cdot ELR \cdot S_{21N} \cdot S_{12N}}$$

where a normalized S-parameter is defined as

$$S_{11N} = \frac{S_{11M} - EDF}{ERF}, \quad S_{21N} = \frac{S_{21M} - EXF}{ETF}, \quad S_{12N} = \frac{S_{12M} - EXR}{ETR}, \quad S_{22N} = \frac{S_{22M} - EDR}{ERR}$$



# Significance of Calibration

## TYPES OF CALIBRATION

### UNCORRECTED



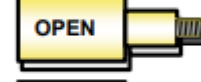
- Convenient
- Generally not accurate
- No errors removed

### RESPONSE



- Easy to perform
- Use when highest accuracy is not required
- Removes frequency response error

### 1-PORT



- For reflection measurements
- Need good termination for high accuracy with 2-port devices
- Removes these errors:
  - Directivity
  - Source match
  - Reflection tracking

### FULL 2-PORT



Defined Thru or Unknown Thru



- Highest accuracy
- Removes these errors:
  - Directivity
  - Source/load match
  - Reflection tracking
  - Transmission tracking
  - Crosstalk (limited by noise)

### ENHANCED RESPONSE

- Combines response and 1-port
- Corrects source match for transmission measurements

# Using Known Standards to Correct for Systematic Errors

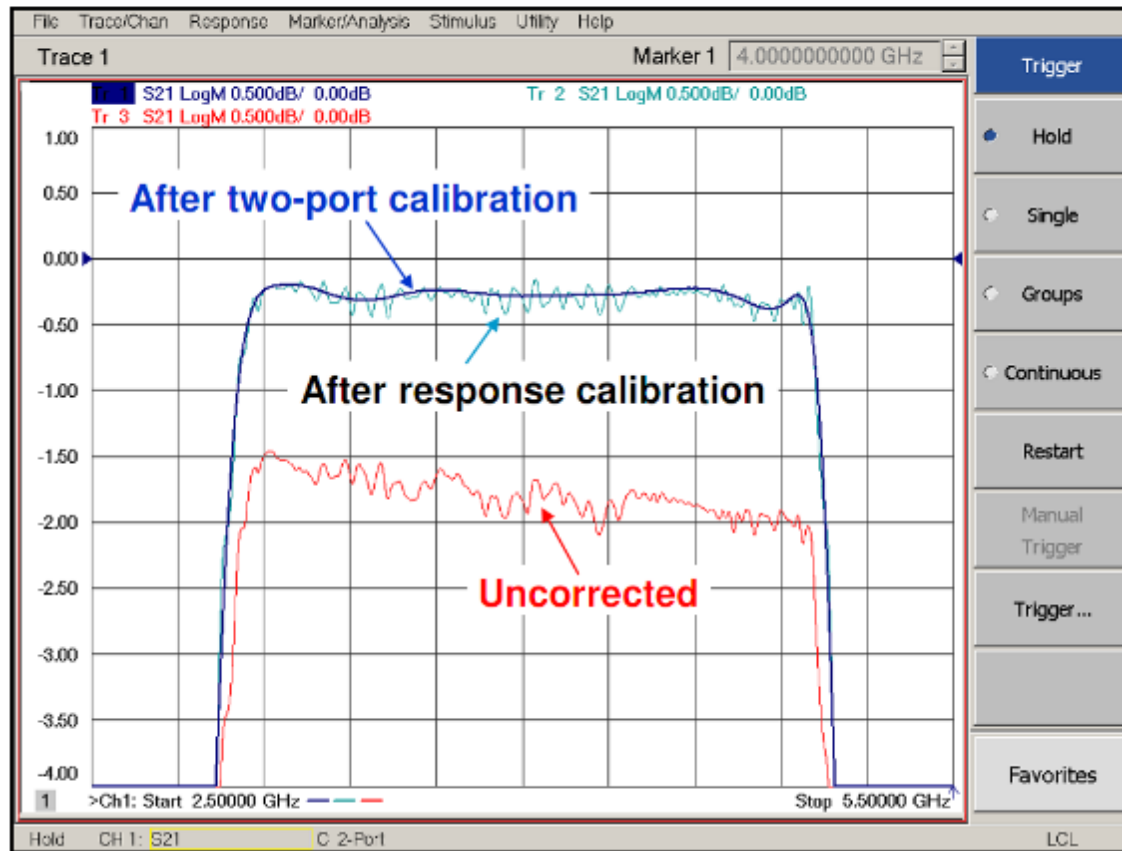
- **Response calibration (normalization)**
  - Only one systematic error term measured
  - Reflection tracking
- **1-port calibration (*reflection measurements*)**
  - Only three systematic error terms measured
  - Directivity, source match, and reflection tracking
- **Full two-port calibration (*reflection and transmission measurements*)**
  - Twelve systematic error terms measured
  - 10 measurements on four known standards (SOLT)
  - 7 measurements using Unknown Thru; 4 measurements using QSOLT
- **Standards defined in cal kit definition file**
  - Network analyzer contains standard cal kit definitions
  - **CAL KIT DEFINITION MUST MATCH ACTUAL CAL KIT USED!**
  - User-built standards must be characterized and entered into user cal-kit




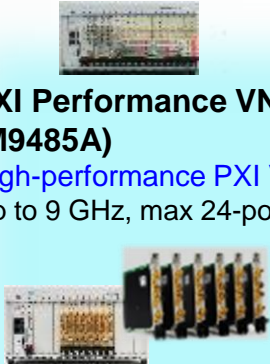




# VNA showing Band Pass Filter

UNCALIBRATED, RESPONSE CAL AND FULL 2 PORT CAL

## Measuring filter insertion loss



# Vector Network Analyzers Product Portfolio

| Handheld VNA   | Modular VNA  | Benchtop VNA   | Accessories   |
|--|--|--|---|
|  <p><b>FieldFox</b><br/>Carry precision with you<br/>30 k to 50 GHz</p> |  <p><b>PXI Performance VNA (M9485A)</b><br/>High-performance PXI VNA<br/>Up to 9 GHz, max 24-ports</p> <p><b>One-slot PXI VNA (M937xA)</b><br/>Drive down the cost of size<br/>Up to 26.5 GHz, max 32-ports</p> |  <p><b>PNA</b><br/>Reach for unrivaled excellence<br/>300 k to 1.5 THz</p> <p><b>ENA</b><br/>Drive down the cost of test<br/>5 Hz to 20 GHz</p> | <p><b>Cal kits (Mech., E-Cal)</b><br/>Up to 120 GHz</p>  <p><b>Accessories-</b> Attenuator, Switch, Coupler, Splitter, etc.</p>  <p><b>Power meter / sensor</b></p>  |

**Industry Broadest Price / Performance Choices** 

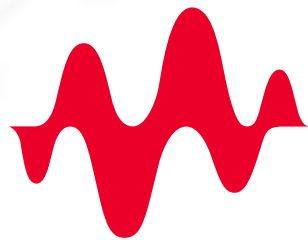
## Software Applications

Ease-of-use, fundamental/advanced applications  
Common VNA software platform  
Flexibility in license types

# Network Analyzer Measurement Resources

- Keysight RF and Digital Monthly Webcast Series [www.keysight.com/find/webcastseries](http://www.keysight.com/find/webcastseries)
  - Live and On Demand Viewing
  - Register for Future Webcasts
- Keysight RF Learning Center [www.keysight.com/find/klcrf](http://www.keysight.com/find/klcrf)
  - Webcast Recordings
  - Application Notes
    - Understanding the Fundamentals of Network Analysis





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